

Turbulent Flows
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Solution to Exercise 6.35

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In simple turbulent shear flow, the only non-zero mean velocity gradient is $\partial \langle U_i \rangle / \partial x_j$. Combining this knowledge with $\mathcal{P} \equiv -\langle u_i u_j \rangle \partial \langle U_i \rangle / \partial x_j$ (Eq.5.133), the production rate of turbulent kinetic energy is given by

$$\mathcal{P} \equiv -\langle u_1 u_2 \rangle \partial \langle U_1 \rangle / \partial x_2. \quad (1)$$

Substituting the given expressions $\mathcal{S} = \partial \langle U_1 \rangle / \partial x_2$ and $\alpha \equiv -\langle u_1 u_2 \rangle / k$ in $\mathcal{S}k/\varepsilon$, and using Eq.(1) it is shown that

$$\begin{aligned} \mathcal{S}k/\varepsilon &= -\frac{\partial \langle U_1 \rangle}{\partial x_2} \frac{\langle u_1 u_2 \rangle}{\alpha} \frac{1}{\varepsilon} \\ &= \frac{1}{\alpha} \frac{\mathcal{P}}{\varepsilon} \approx 3, \end{aligned} \quad (2)$$

where the numeric result is obtained by substituting the given values $\mathcal{P}/\varepsilon \approx 1$ and $\alpha \approx 0.3$.

By using the Kolmogorov timescale $\tau_\eta = (\nu/\varepsilon)^{1/2}$ (Eq.6.3), Eq.(2) and the definition of the turbulence Reynolds number $\text{Re}_L \equiv k^{1/2}L/\nu$ (Eq.6.59) it is shown that

$$\begin{aligned} \mathcal{S}\tau_\eta &= \frac{1}{\alpha} \frac{\mathcal{P}}{\varepsilon} \frac{\varepsilon}{k} \left(\frac{\nu}{\varepsilon} \right)^{1/2} \\ &= \frac{1}{\alpha} \frac{\mathcal{P}}{\varepsilon} \left(\frac{\varepsilon\nu}{k^2} \right)^{-1/2} \\ &= \frac{1}{\alpha} \frac{\mathcal{P}}{\varepsilon} (\text{Re}_L)^{-1/2} \approx 3\text{Re}_L^{-1/2}. \end{aligned} \quad (3)$$

When the relation between the turbulence and the Taylor-scale Reynolds numbers $\text{R}_\lambda = \left(\frac{20}{3} \text{Re}_L \right)^{1/2}$ (Eq.6.64) is substituted in the result from Eq.(3),

it is obtained that

$$\begin{aligned}
\mathcal{S}\tau_\eta &= \frac{1}{\alpha} \frac{\mathcal{P}}{\varepsilon} (\text{Re}_L)^{-1/2} \\
&= \frac{1}{\alpha} \frac{\mathcal{P}}{\varepsilon} \left(\frac{3}{20} \text{R}_\lambda^2 \right)^{-1/2} \\
&= \sqrt{\frac{20}{3}} \frac{1}{\alpha} \frac{\mathcal{P}}{\varepsilon} \text{R}_\lambda^{-1} \approx 9 \text{R}_\lambda^{-1}.
\end{aligned} \tag{4}$$

Using the definition of the length scale L_S from Eq.(6.272), the solution of Eq.(2) and the definition of the lengthscale $L \equiv k^{3/2}/\varepsilon$ characterizing the large eddies, it is shown that

$$\begin{aligned}
L_S &\equiv \mathcal{S}^{-3/2} \varepsilon^{1/2} \\
&= \left(\frac{\mathcal{P}}{\alpha k} \right)^{-3/2} \varepsilon^{1/2} \\
&= \frac{\mathcal{P}^{-3/2}}{\alpha^{-3/2}} \varepsilon^{1/2} L \varepsilon \\
&= \left(\frac{\mathcal{P}}{\varepsilon} \right)^{-3/2} \alpha^{3/2} L \approx \frac{1}{6} L.
\end{aligned} \tag{5}$$

Finally, by substituting the result of Eq.(2) in the definition of the velocity scale u_S from Eq.(6.276), it is shown that

$$\begin{aligned}
u_S &\equiv (\varepsilon/\mathcal{S})^{1/2} \\
&= \left(\frac{\varepsilon \alpha k}{\mathcal{P}} \right)^{1/2} \\
&= \alpha^{1/2} \left(\frac{\mathcal{P}}{\varepsilon} \right)^{1/2} k^{1/2} \approx \frac{1}{2} k^{1/2}.
\end{aligned} \tag{6}$$

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